

Voltage Ratio and Impedance Calculations for Coupled Inductors and Autotransformers

Ref. Electronic Engineering by Alley & Atwood p. 324
Coupled Inductors

https://en.wikipedia.org/wiki/Inductance#Mutual_inductance

Portland University ECE221 Magnetically Coupled Circuits

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General Equations for Coupled Inductors

$$\begin{pmatrix} V_1 \\ V_2 \end{pmatrix} = \begin{pmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{pmatrix} \cdot \begin{pmatrix} I_1 \\ I_2 \end{pmatrix}$$

V_x = voltages
 Z_{xx} = Impedances
 I_x = currents

$$V_1 = Z_{11} \cdot I_1 + Z_{12} \cdot I_2$$

$$V_2 = Z_{21} \cdot I_1 + Z_{22} \cdot I_2$$

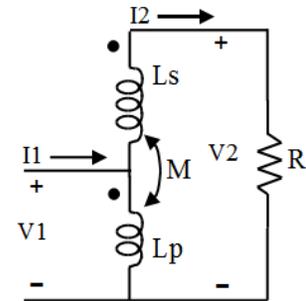
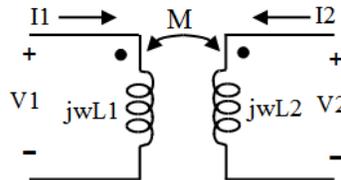
Calculation of Z_{in} by setting $V_2 = 0$

$$0 = Z_{21} \cdot I_1 + Z_{22} \cdot I_2$$

$$I_2 = -\frac{I_1 \cdot Z_{21}}{Z_{22}}$$

$$V_1 = Z_{11} \cdot I_1 + Z_{12} \cdot I_2$$

$$V_1 = \frac{I_1 \cdot (Z_{11} \cdot Z_{22} - Z_{12} \cdot Z_{21})}{Z_{22}}$$



$$Z_{in1} = \frac{Z_{11} \cdot Z_{22} - Z_{12} \cdot Z_{21}}{Z_{22}}$$

General equation for Z_{in} at port 1

For separate coupled inductors:

$$Z_{11} = j \cdot \omega \cdot L_1$$

$$Z_{12} = Z_{21} = j \cdot \omega \cdot M$$

$$Z_{22} = R + j \cdot \omega \cdot L_2$$

Where M is the mutual inductance for both cases

For both cases, with K = coupling coeff.

$$M = K \cdot \sqrt{L_1 \cdot L_2}$$

For the Autotransformer:

$$Z_{11} = j \cdot \omega \cdot L_1$$

$$Z_{12} = Z_{21} = -j \cdot \omega \cdot (L_1 + M)$$

$$Z_{22} = R + j \cdot \omega \cdot L$$

R = Load resistance at secondary

Notes:

The negative sign of Z_{12} and Z_{21} is used since i_2 flows out of the polarity mark

$$L = L_1 + L_2 + 2 \cdot M \quad \text{Inductance at output}$$

Exemple of Calculation of Zin1: R is on the secondary side (V2) for the autotransformer

$N := 6$ Turns ratio of L2 to L1 $N_{eff} := N + 1$ Effective turns ratio of autotransformer
 $L1 := 3$ $L2 := N^2 \cdot L1$ $R := 50 \cdot N_{eff}^2$ $K := 0.95$ $M := K \cdot \sqrt{L1 \cdot L2}$ $L_{ww} := L1 + L2 + 2 \cdot M$
 R value chosen to reflect 50 ohms at input: $R = 2450$

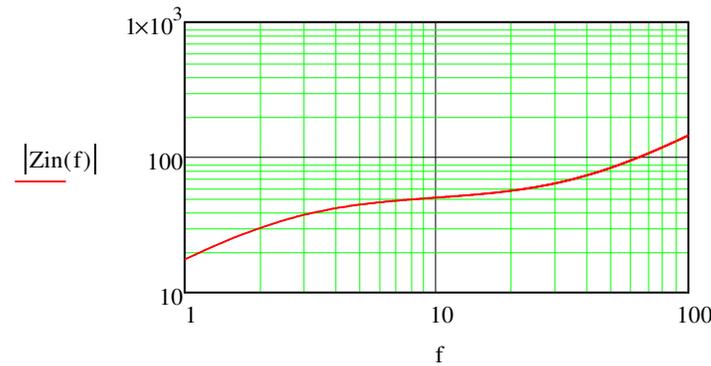
$f := 1, 1.1.. 100$ F in MHz and L, M in μH
 $w(f) := 2 \cdot \pi \cdot f$

$Z11(f) := j \cdot w(f) \cdot L1$
 $Z12(f) := -j \cdot w(f) \cdot (L1 + M)$
 $Z21(f) := Z12(f)$
 $Z22(f) := R + j \cdot w(f) \cdot L$

NOTE :
 Interchanging L1 and L in Z11 and Z22 will calculate Zin2 (secondary side) with R on the primary side (V1)

$Zin(f) := \frac{Z11(f) \cdot Z22(f) - Z12(f) \cdot Z21(f)}{Z22(f)}$

General equation for Zin at port 1 (input)



$|Zin(1)| = 17.671$
 $|Zin(10)| = 50.639$
 $|Zin(100)| = 145.717$

Calculation of Av, the voltage transfer ratio

$V1 = Z11 \cdot I1 + Z12 \cdot I2$
 $V2 = Z21 \cdot I1 + Z22 \cdot I2$

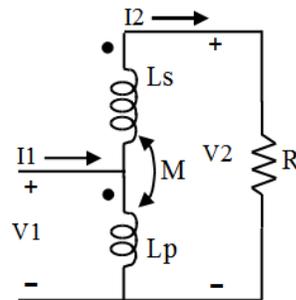
With $V2=0$ Calculate $Av = V2 / V1$
 R is on the sec. (V2)

$0 = Z21 \cdot I1 + Z22 \cdot I2$
 $I1 = -\frac{I2 \cdot Z22}{Z21}$ Solve for I1

$V1 = Z11 \cdot I1 + Z12 \cdot I2$

$V1 = -\frac{I2 \cdot (Z11 \cdot Z22 - Z12 \cdot Z21)}{Z21}$

Recall that: $Av = \frac{I2}{V1} \cdot R$



$Av = \frac{Z21 \cdot R}{Z12 \cdot Z21 - Z11 \cdot Z22}$

General equation for $Av = V2 / V1$. This is NOT insertion loss !

Example, usint the same values as previous example

$$L1 = 3 \quad L2 = 108 \quad R = 2.45 \times 10^3 \quad K = 0.95 \quad M = 17.1 \quad L = 145.2$$

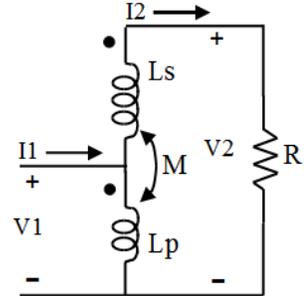
$$Z_{11}(f) := j \cdot \omega(f) \cdot L1$$

$$Z_{12}(f) := -j \cdot \omega(f) \cdot (L1 + M)$$

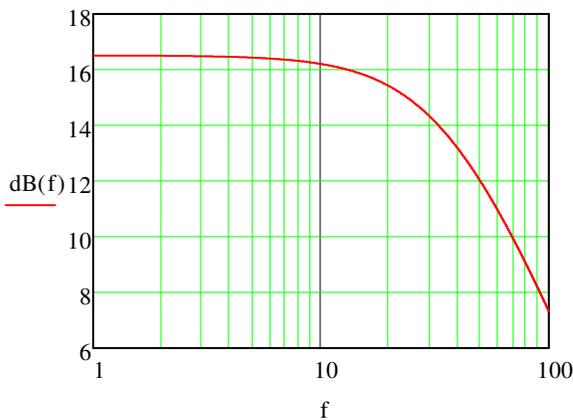
$$Z_{21}(f) := Z_{12}(f)$$

$$Z_{22}(f) := R + j \cdot \omega(f) \cdot L$$

NOTE :
Interchanging L1 and L in Z11 and Z22 will calculate V1 / V2 with R on the primary side (V1)



$$Av(f) := \frac{Z_{21}(f) \cdot R}{Z_{12}(f) \cdot Z_{22}(f) - Z_{11}(f) \cdot Z_{22}(f)} \quad dB(f) := 20 \cdot \log(|Av(f)|)$$



$$|Av(1)| = 6.698$$

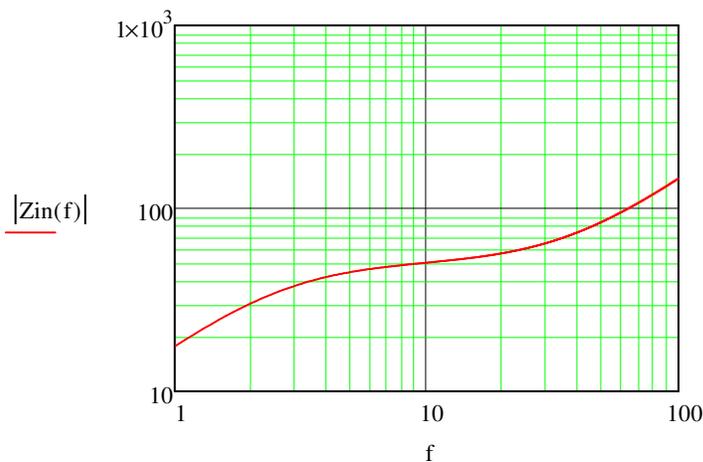
$$|Av(10)| = 6.468$$

$$|Av(100)| = 2.327$$

With the coupling coefficient $K = 1$, the Av ratio = 7

Zin and SWR Calculation at Input

$$Z_{in}(f) := \frac{Z_{11}(f) \cdot Z_{22}(f) - Z_{12}(f) \cdot Z_{21}(f)}{Z_{22}(f)}$$



$$|Z_{in}(1)| = 17.671$$

$$|Z_{in}(10)| = 50.639$$

$$|Z_{in}(100)| = 145.717$$

$$Z_{in}(1) = 5.717 + 16.721i$$

$$Z_{in}(10) = 43.791 + 25.43i$$

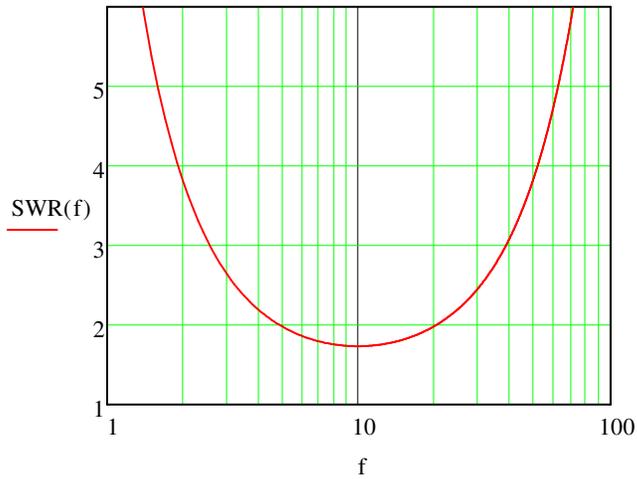
$$Z_{in}(100) = 46.915 + 137.958i$$

SWR Calculation based on Zin, at input

$Z_0 := 50$

$$SWR(f) = \frac{1 + \left| \frac{Z_{in}(f) - Z_0}{Z_{in}(f) + Z_0} \right|}{1 - \left| \frac{Z_{in}(f) - Z_0}{Z_{in}(f) + Z_0} \right|}$$

$$SWR(f) := \frac{2 \cdot |Z_0 + Z_{in}(f)|}{|Z_0 + Z_{in}(f)| - |Z_0 - Z_{in}(f)|} - 1$$



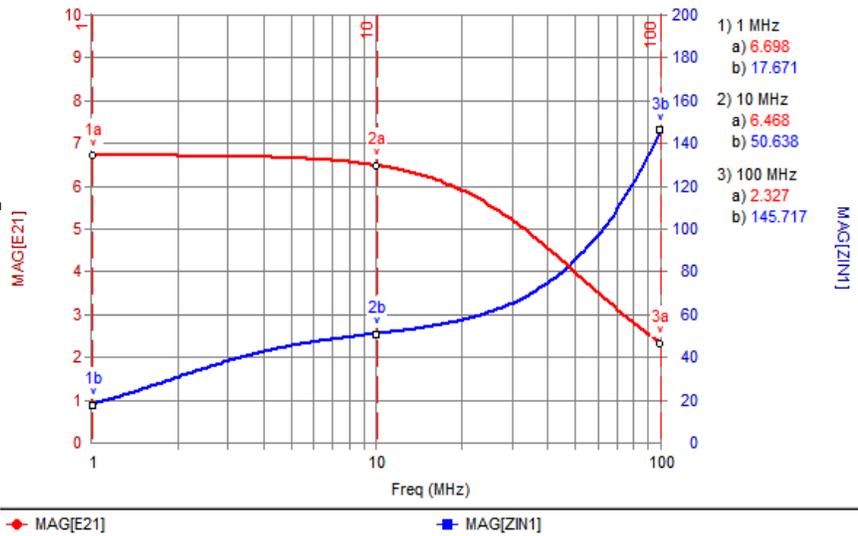
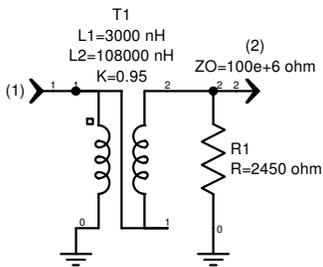
$SWR(3.5) = 2.372$

$SWR(10) = 1.737$

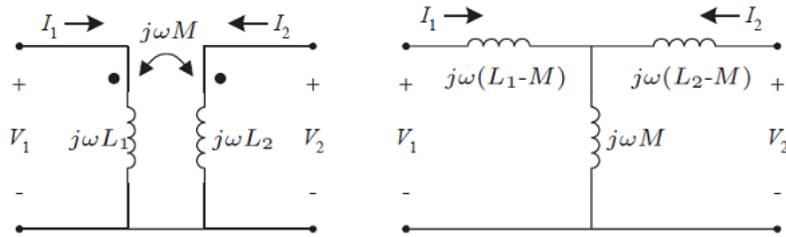
$SWR(29) = 2.422$

Ref: IndependantCoupledCoils-VS-Tapped coil-1.wsp

Simulations



Phasor Analysis: T-Equivalent



Frequency Domain (Phasors)

$$\begin{aligned} V_1 &= j\omega L_1 I_1 + j\omega M I_2 \\ V_2 &= j\omega M I_1 + j\omega L_2 I_2 \end{aligned}$$

- The T-equivalent is only valid if bottom terminals are connected

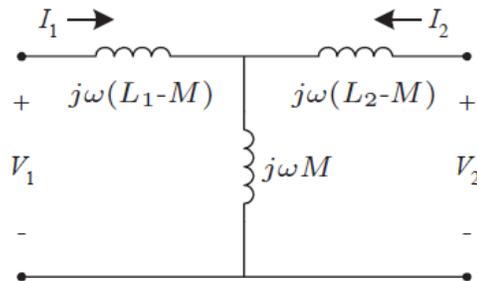
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Equivalent Tee circuit for Independent Inductors

$$Z_{11} = j \cdot \omega \cdot L_1$$

$$Z_{12} = Z_{21} = j \cdot \omega \cdot M$$

$$Z_{22} = R + j \cdot \omega \cdot L_2$$



Equivalent Tee Circuit for the Autotransformer

For the Autotransformer:

$$Z_{11} = j \cdot \omega \cdot L_1$$

$$Z_{12} = Z_{21} = -j \cdot \omega \cdot (L_1 + M)$$

$$Z_{22} = R + j \cdot \omega \cdot L$$

From comparisons with the independent inductor Tee circuit above

$$L_a = L_1 - (L_1 + M)$$

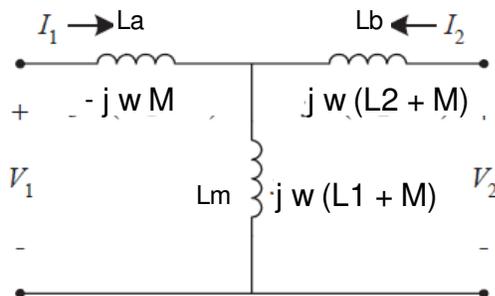
$$L_b = L - (L_1 + M) = L_2 + M$$

$$L_m = L_1 + M$$

$$M = K \cdot \sqrt{L_1 \cdot L_2}$$

$$L = L_1 + L_2 + 2 \cdot M$$

Autotransformer equivalent Tee circuit



Example, using the same values as in page 3:

$$L1 := 3 \quad L2 := 36 \cdot L1 \quad R := 2450 \quad K := 0.95 \quad M := K \cdot \sqrt{L1 \cdot L2} \quad L := L1 + L2 + 2 \cdot M$$

M and L can be calculated:

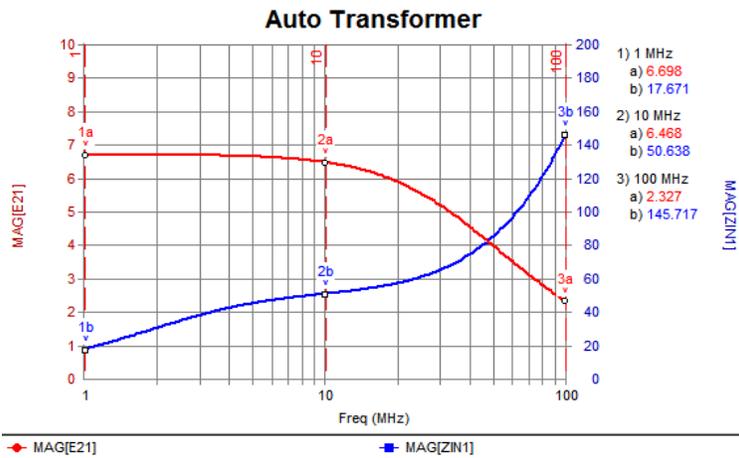
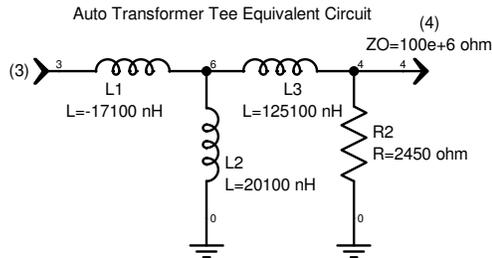
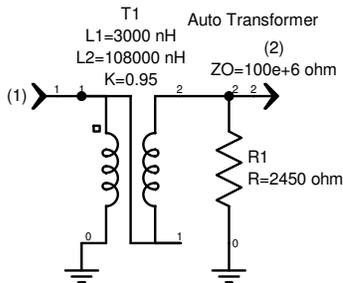
$$M := K \cdot \sqrt{L1 \cdot L2} = 17.1 \quad L := L1 + L2 + 2 \cdot M = 145.2$$

Tee Equivalent circuit:

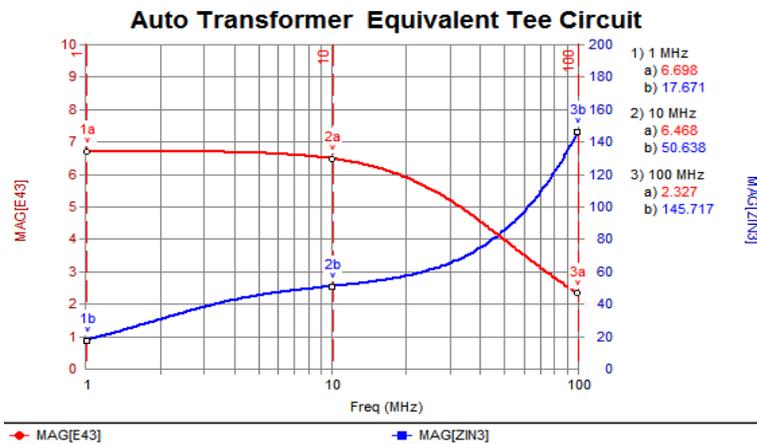
$$La := -M = -17.1$$

$$Lb := L2 + M = 125.1$$

$$Lm := L1 + M = 20.1$$



AutoTransformer Simulation



AutoTransformer Tee Equivalent Circuit Simulation

Voltage Gain Variation vs Coupling Coefficient K

With $K = 1$ (perfect coupling) the low frequency gain = 7.00

With $K = 0.95$ the low frequency gain = 6.698 (dotted curves)

With $K = 0.90$ the low frequency gain = 6.391 (solid curves)

